P/034/61/000/012/003/003 D265/D305

CONTRACTOR DESCRIPTION

Application of transistorized ...

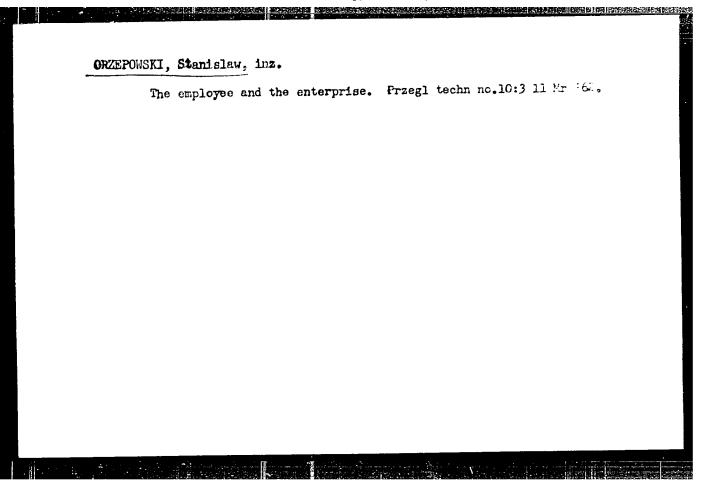
oscillograph. The methods of taking the measurements, their accuracy and precautions to be observed in order to eliminate the influence of non-linear characteristics of the amplifier and the interference are described in this paper. This method permits the study of commutation, the instantaneous values of e.m.f of d.c. machines and the temperature increase of armatures. Photographs are included of the CRO's graphs. There are 11 figures.

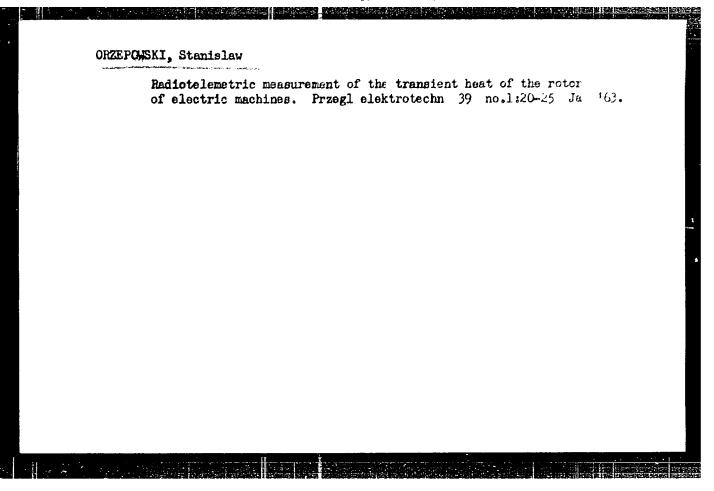
Card 2/2

ORZEPOWSKI, Stanislaw, inz.

Annual of the property of the

Worker and institution; a discussion of professional ethics. Przegl techn no.10:3 162.





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ORZESKI, 5.

Rural smithy. p. 27

BUDOWNICTMU MIEDIALE. (Ministerstwo Rolnictwa i ministerstwo Panstwowych Gospodarstw Rolnych) Marszawa, Poland. Vol. 11, no. 10, oct. 19,7

Monthly list of East European Accessions (MEAI) LC, Vol. 9, no. 2, rev. 1760

Uncl.
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s/058/62/000/009/059/069 A057/A101

AUTHOR:

Orzeszek, J. S.

TITLE:

Focusing system for traveling wave tubes

PERIODICAL: Referativnyy zhurnal, Fizika, no. 9, 1962, 26 - 27, abstract 9-3-52ch ("Prace Przemysł. inst. telekomun", 1961, v. 11, no. 35, 17 - 24,

Polish; summaries in Russian, English and French)

The Przemysl Institute for Telecommunications (Poland) carried out a detailed investigation of focusing systems, constructed from copper wire coils and aluminum foils. A complete method is developed for calculating the system with consideration of constructive tolerances and temperature limitations. It is shown that for the necessary conditions of focusing a winding of elliptical cross section and side coils must be used. Coils of aluminum foil have a simple design, relatively small dimensions (in view of a considerably greater filling coefficient), and an easy heat removal. Interturn insulation is ensured by a varnish film. The simplicity of design permits application of magnetic screens for adjusting its characteristics. Cooling of focusing systems can be performed

Card 1/2

# "APPROVED FOR RELEASE: Wednesday, June 21, 2000 CIA-

CIA-RDP86-00513R001238

S/058/62/000/009/059/069 A057/A101

Focusing system for traveling wave tubes

by means of radiator plates and air current. Tables are presented, showing the advantages of aluminum foil application. There are 2 references.

N. S.

[Abstracter's note: Complete translation]

Card 2/2

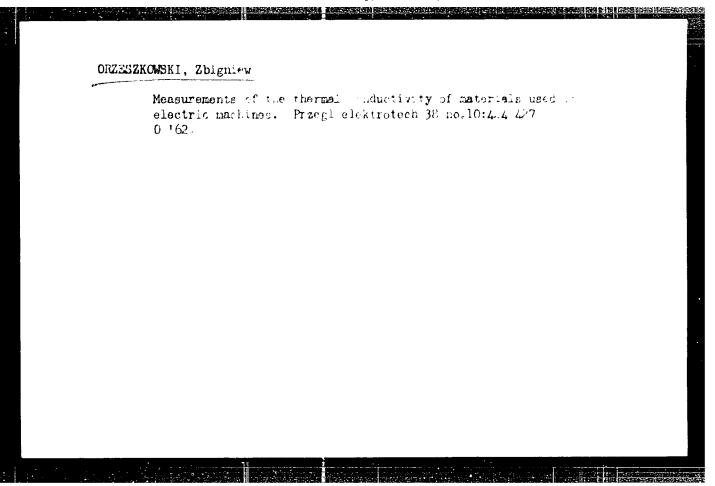
20 mm - 7. ĸ POLIMD/Ortics - Photography Als Jour : Ref Zhur Fizika, No  $\theta$ , 1959, 192 $\delta$ 7 Author : Stronczak, Wojcieck. Orzeszko, Witold Inst Title : Xerography Orig Pub : Hutnik (Polska), 1950, 25, No 7-8, 307-310 Abstract : Popular article. Card 1/1

Chricanoraki, n.; Armanirroka, F.

Calorimetric method of measuring the efficiency of asynchronous motors could by vator.  $p_{\bullet}$  (7.

RCTFR: Y ELUCTROTECHNING F. (b. 1848 Akademia Naum, Instytut Lader wych możlemow Techniki) Tarszawa, ieland. Vel. 5. No. 1, 1059.

Minthly List of last bur pean accession (TAI), LC. Vol. 3, NC. 9, September, 1959. Uncl.



ORZESZKOWSKI, Zbigniew, dr inz.

Temperature measurements of turbogenerator rotors. Przegl elektrotechn 40 no.5:230-232 My '64.

1. Department of Electric Measurements, Technical University, Wroclaw.

くない けんさんかく

112-1-1304

Translation from: Referativnyy Zhurnal, Elektrotekhnika, 1957,

Nr 1, p.200 (USSR)

AUTHOR:

Orzhakhovskiy, M.L.

TITLE:

Bar Thermoregulator (Sterzhnevoy termoregulyator)

PERIODICAL: Sbornik.rats. predlozheniy, M-vo elektrotekhn, prom-sti SSSR, 1955, Nr 56, pp.7-8.

ABSTRACT:

A simple dilatometric temperature regulator in thermestats and furnaces for baking commutators, plastic and other parts, is presented; it provides ± 10° limits of regulation. An aluminum bar is permanently fixed at one end in an asbestos-cement plate with lead monoxide, and at the other free end it pushes against the short arm of the lever. A silver contact is placed on the long arm of the

Card 1/1

lever and a contact screw is fixed opposite it.

G.I.F.

307-28-18-4- 4 75

AUTHORS:

Bajev, V.A., and Grzhakhovskiy, M.I., Engineers

TITLE:

Classification of Electric Insulating Materials (1960) spect to Heat Resistance (Klassifikatsiya elektri.zo.yot-

sionnykh materialov po nagrevostcykosti)

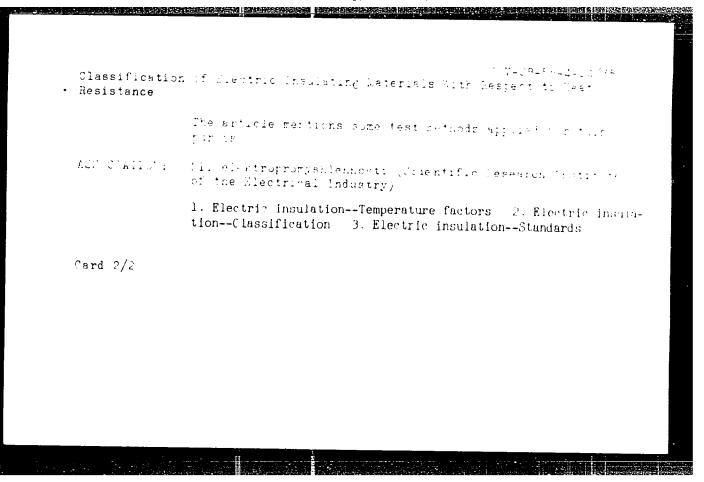
FERIODICAL:

Standartizatsiya, 1959, Nr 4, pp 76 - 79 (1974)

ABSTRACT:

The development of new electric insulating materials bequired the revision of existing classification. New atomiards of insulating materials for electric machines, devices and transformers have been approved as well as their plane sification with respect to heat resistance. The importance of the new standard consists in the clear determination of limit temperatures in the continuous utilization of limit ation in electric equipment. The new DBT standard wire plies with scientific, technical and industrial requirements. The issue of the standard will entail some modifications and additins relating to the existing standards. Clare.lication of the new materials is based or experimental test methods in advordance with the law of Newt-aging.

Card 1/2



BAYEV, V.A., inzh.; MASLOV, V.V., inzh.; ORZHAKHOVSKIY, M.L., inzh.

Performance of electrical equipment designed for operation in tropical climates. Vest. elektroprom. 33 no.7:30-35 Jl '62.

(MIRA 15:11)

(Electric apparatus and appliances)

KUZNETSOV, B.I., inzh.; ARTANOV, S.G., kand.tekhn.nauk; ORZHAKHOVSKIY,
M.L., inzh.

Principal factors determining the reliability of electrical
machines. Vest. elektroprom. 33 no.9:57-62 S 62. (MIRA 15:10)
(Electric machinery)

DESCRIPTION OF THE PROPERTY OF

ACCESSION NR: AT4017006

8/3057/63/000/000/0158/0164

AUTHOR: Tikhomirov, V. B.; Orzhakhovskiy, M. L.

TITLE: Basic principles of rapid testing of polymer shieldings for durability

SOURCE: Zashchitny\*ye pokry\*tiya v atomnoy tekhnike (Shielding in nuclear engineering); sbornik statey. Moscow, Gosatomizdat, 1963, 158-164

TOPIC TAGS: atomic reactor shielding, polymer shielding, shielding, atomic reactor, nuclear shielding, shielding durability, oxidation, corrosion, radioactivity

ABSTRACT: In a previous publication (Laboratornaya metodika opredeleniya dolgovechnosti polimerny\*kh pokry\*tiy v zhidkikh agressivny\*kh sredakh. Sm. Nast. sb., str. 166), the authors designed a test to determine the rated life of shielding in aggressive media. In the present paper, the principles behind such determinations are reviewed. Accurate estimation of the practical value of polymer shieldings can be made on the basis of durability. Chemical reactions such as polymerization and depolymerization change the properties of polymer shieldings. In addition, oxidation, corrosion, and chemical de-

Card 1/2

ACCESSION NR: AT4017006

composition lead to similar results. Physical processes acting in the same way include liberation of the components, cracking, wear, and sorption and desorption of radioactive substances. For the design of tests, all the abovementioned factors must be included in the test cycles in order to determine the rated life of the shieldings.

ASSOCIATION: None

SUBMITTED: 00

DATE ACQ: 20Feb64

ENCL: 00

SUB CODE:

NP

NO REF SOV: 001

OTHER: 000

Card 2/2

ACCESSION NR: AT4017007

\$/3057/63/000/000/0165/0172

AUTHOR: Orzhakhovskiy, M. L.; Tikhomirov, V. B.

TITLE: Laboratory methods for determining the durability of polymer shieldings in aggressive liquid media

SOURCE: Zashchitnywye pokrywtiya v atomny tekhnike (Shielding in nuclear engineer-ing); sbornik statey. Moscow, Gosatomizdat, 1963, 165-172

TOPIC TAGS: atomic reactor, shielding, nuclear shielding, polymer shielding, shielding durability, reactor shielding

ABSTRACT: A testing method is described for determining the durability of polymer shieldings under the influence of acids, alkalies, and soaps. Shieldings working under these conditions should protect the underlying metal or concrete against corrosion. The testing conditions should be even more severe than the working conditions. Thus, the testing is performed at higher temperatures and concentrations than those under working conditions. Since the electrical resistance of the film shows, to some extent, whether it will remain as a protective coating, the testing device consists essentially of an ohmmeter (see Fig. 1 of the Enclosure). The tests show that the logarithm of the life of the shielding is directly proportional to the reciprocal of the absolute temperature. This is also true for ard 1/3

ACESSION NR: AT4017007

epoxy shielding. The main phenomenon showing deterioration of the shielding is the dissolution of the protected metal in the aggressive media. Orig. art. has: 2 figures and 10 equations.

ASSOCIATION: none

SUBMITTED: 00

DATE ACQ: 20Feb64

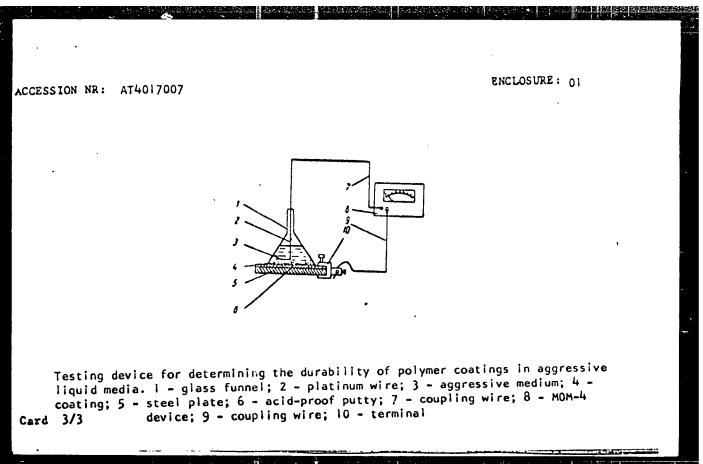
ENCL: 01

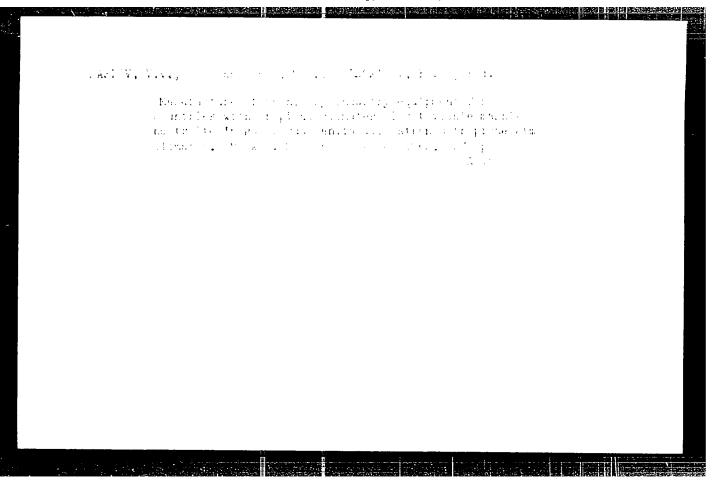
SUB CODE: NP, OC

NO REF SOV: 002

OTHER: 000

Card 2/3





16

L 18008-66 EWT(m)/EWP(j)/T/EWP(t) JD/WW/WB/RM Source CODE: UR/0303/65/000/005/0052/0057 ACC NR: AP6004319

AUTHOR: Orzhakhovskiy, H. L.; Zvyagintseva, N. V.

ORG: none

TITLE: The relation of the thickness of epoxy and polyester coatings on metals and concrete to their durability in liquid corrosive media

SOURCE: Lakokrasochnyye materialy i ikh primeneniye, no. 5, 1965, 52-57

TOPIC TAGS: protective coating, epoxy plastic, polyester plastic, lacquer

ABSTRACT: A study was made of the characteristics of self-dried coatings based on a polyethylenepolyamine-cured epoxy lacquer (CHS-epoxy-2000 resin and dibutyl phthalate in the ratio of 10:1) and on PE-214 polyester lacquer. The coatings were applied on steel surfaces (cleaned by blasting with metal shot) and on plastered concrete surfaces. The porosity of the coatings was determined from their electrical resistance and changes in this resistance under the action of water. It is pointed out that the porosity of epoxy and polyester coatings is unsatisfactory in the resistance drops by 2 to 5 orders of magnitude in 24 hr. The lower limit of the

UDC: 667.613.3

Card 1/2

L 18008-66 ACC NR: AP5004319

thickness of epoxy and polyester coatings (also known as the critical thickness) was found to be 100-110µ on shot-blasted steel surfaces, 25-50µ on untreated surfaces of thin-sheet steel, and 240-300µ on the surface of plastered concrete. The durability of a coating in liquid corrosive media is determined by its working thickness. For metal coating, this thickness is the difference between the total and critical thickness, and for coatings on concrete, the total thickness of the coating. For epoxy and polyester coatings, there is a direct relation between the service life and the working thickness. This makes it possible to adopt the specific service life of a coating (expressed in units of time (hr) per 100µ of its working thickness) as a measure of its durability. Orig. art. has: 10 figure, 1 table.

SUB CODE: 11/ SUBM DATE: 00/ ORIG REF: 005/ OTH REF: 002

Card 2/2 mgs

# "APPROVED FOR RELEASE: Wednesday, June 21, 2000

CIA-RDP86-00513R001238

L 456°5-66 EVT (m)/FVP(1)/T/EWP(t)/ETI IJP(c) JD/WB/RM

ACC NR. AP6024053 (A) SOURCE CODE: UR/0191/66/000/005/0060/0065

AUTHOR: Orzhakhovskiy, M. L.

ORG: none

TITLE: Relationships governing the influence of the temperature and concentration of a corrosive medium on the service life of polymeric materials

SOURCE: Plasticheskiye massy, no. 5, 1966, 60-65

TOPIC TAGS: durability, polymer stability, corrosion resistance, protective coating

ABSTRACT: A series of regularities reported earlier by the author formed the basis for a method of testing the service life of polymeric coatings. Some additional results of these studies are given in the present paper. It is shown that independently of the process by which the polymer is attacked, the log of the service life is inversely proportional to the absolute temperature, this relationship being expressed by a straight line. From the latter, the service lives of coatings can be determined at any temperature of a corrosive medium of a given concentration. This makes it possible to accelerate the tests for service life by raising their temperature, then extrapolating the results to lower (working) temperatures. Experimental data confirmed these relationships. The life of a polymeric coating as a function of the concentration of a corrosive agent should not be expressed in units of time, but by the ratio of the life in question to the life at some definite concentration of the corrosive agent,

Card 1/2

UDC: 678,019,34

f	or exa	example, 30%. A procedure for rapidly testing the life of polymers, based on the regoing considerations, is described. Orig. art. has: 7 figures and 14 formulas.										
	_	_	,,		rood, olik	· arc.	nası 7 I	igures and 14 formulas				
		11/	SUBM DATE:	none/	OKTO KELI	003/	OTH REF:	001				

ORLOVA, M.P.; ORZHDESTVINSKIT, Yu.P.: BARANOVA, Ye.R.

Mineralogy of the mare-meta, mandomatites of the Sallamiatvinskii Massif (northern Kardila), Truly VS.S.I. #6:3-20 163.

(MI A 17:4)

s/137/62/000/003/185/191 A154/A101

AUTHORS:

Yatsyk, I. Ye.; Orzhekhovskaya, A. I.

TITLE:

Determination of cerium in iron-based alloys

PERIODICAL: Referativnyy zhurnal, Metallurgiya, no. 3, 1962, 6, abstract 3 K 27 ("Sb. nauchno-tekhn. tr. N.-i. in-t metallurgii Chelyab sovnarkhoza".

i961, vyp. 3, 205 - 210)

A method was proposed for photocolorimetric determination of Ce in a Fe-based alloy in amounts of 0.01 - 1.0 %. 1 g of steel was dissolved in a TEXT: 100-ml retort in 20 ml of HCl, oxidized by HNO3, evaporated twice with 10 ml of HCl, another 10 ml of HCl was added, and the contents were evaporated until moist salts were obtained. The solution was transferred to a separating funnel, and concentrated HCl, saturated with ethyl ether (5 - 6 ml of acid per 1 g of Fe). and 30 ml of ethyl ether were added. The ether layer was separated from the water layer. The funnel was rinsed with 5 ml of ether-saturated HCl. The solution was allowed to settle, the acid layer combined, and the ether layer thrown away. The Fe-free solution was boiled to remove the ether, concentrated by evaporation, 10 ml of  $H_2SO_4$  was added, and the solution concentrated by evaporation

Card 1/2

Determination of cerium in iron-based alloys

S/137/62/000/003/185/191 A154/A101

until the appearance of  $50_3$  vapors. The salts were dissolved in water, the salts tion was transferred into an Erlenmeyer flask by water, and Cr and Mr. were on alloed by ammonium persulfate in the presence of 20 ml of a 0.25 % solution of AgNCa. A 25 % solution of NH $_4$ OH was added to the cooled solution until an odor was produced, whereby Ce, Fe. Ti and other hydroxides were precipitated. This precipitate was then separated and dissolved in HCl (1:1). The solution was evaporate ed down to 10 ml, 30 ml of a  $Ca(OH)_2$  suspension was added, and the solution even porated dry. It was then twice concentrated by evaporation with 5 ml of HC.. The iry residue was dissolved in 10 ml of HCl, evaporated until moist salts warleft, 15 ml of oxalic acid was added, and the solution diluted to 30 ml with water. The precipitate and the filter were placed into a retort, 10 ml  ${\rm cf}$   ${\rm a}$ mixture of boric and citric acids were added, the solution was filtered. 20  $_{
m max}$ of water was added and the solution was boiled, turning the filter into paper pulp. This pulp was then filtered off, the filtrate evaporated down to 25 ml. cooled, 20 drops of a 1% solution of  ${\rm H}_2{\rm O}_2$  and 15 drops of a 25 % solution of NH4CH were added. The solution was transferred after 15 minutes to a 50 ml retort, diluted with water till it reached the mark, and analyzed on a  $\Phi \mathbb{R} - \mathbb{R}$ (FEK-M) photocolorimeter with a blue light filter.

[Abstracter's note: Complete translation]
Card 2/2

L. Vorob'yeva

APPROVED FOR RELEASE: Wednesday, June 21, 2000

CIA-RDP86-00513R001238

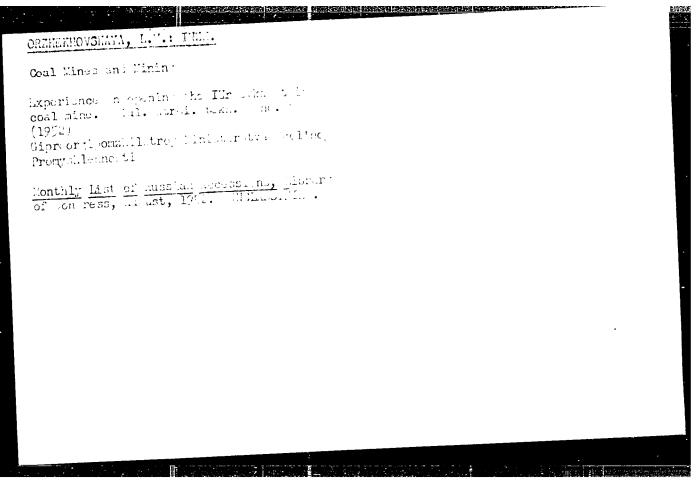
YAKOVIEV, P.Ya.; OR7HEKHOVSKAYA, A.I.

Gas volumetric methods for determining carbon in metals.
Zav.lab. 28 no.10:1267-1269 '62. (MIRA 15:10)

1. TSentral'nyy nauchnq-issledovatel'akiy institut chernoy metal.urgii imeni 1.P.Bardina.
(Carbon—Analysis) (Metals—Analysis)

YAKOVLEV, P.Ya.; ORZHEKHOVSKAYA, A.I.

Determining carbon (0.001 - 0.2 %) in metals, steels, alloys, and ferroalloys by the potentiometric method. Sbor.trud. TSNIICHM no.31:144-150 '63. (MIRA 16:7) (Metals--Analysis) (Carbon--Analysis) (Potentiometric analysis)



OBODOVSKIY, Boris Arnolidovich; KHANIL, Solomon Yerimovich;
Prinimali uchastiye ORZHEKHOVSKAYA, O.P.; ITSKOVICH,
G.M.; DARKOV, A.V., prof., doktor tekhn. nauk,
retsenzent; KRYUKOVSKIY, S.S., prof., retsenzent
[deceased]; KRYTOV, G.M., dots., retsenzent; RAKIVNENKO,
V.N., st. prepod., retsenzent; VINCKUROV, A.I., otv. red.;
VAYNBERG, D.A., red.

[Strength of materials in examples and problems] Sopretivlenie materialov v primerakh i zadachakh. Kharikov, Izdvo Kharikovskogo pos. univ., 1965. 31/. p. (MIMA 18:5)

A CONTRACTOR OF THE PROPERTY O	and the comment of the	idicious properties in	and to the second secon				
ORZIJAKOVSKIY, A. M.	PA 240T52						
ORZIJELNOV SATI, A. P.,	drive of roller mills and other milling machines and mechanisms. Power factor efficiency of motors were increased. Refers to use of selenium synchronizing units VSMN-1000/525 produced by "KIP" Plant of Min of Petroleum Industry. Submitted 17 Sep 51.	"Elektrichestvo" No 5, pp 57-59  Discusses experience of milling combines No 1 at Tbilisi, No 3, and Combine imeni Tsyurupa (latter 2 in Moscow) in synchronizing centralized transmission 240752	"Increasing the Power Factor at Enterprises of the Flour Milling Industry," Engr A. M. Orzhekhovskiy, Main Admin for Production of Flour and Meal, Engr S. G. Emma, Milling Combine imeni Tsyurupa, and Engr I. M. Rabinovich, Milling Combine No 3	USSR/Electricity - Induction Motors May 52			

# ORZHEKHOVSKIY, A. M.

OREHEKHOVSKIY, A., inchener.

Prevention of two-phase operation of three-phase electric motors.

Muk.-elev.prom. 20 no.12:26-27 D 154. (MLRA 8:3)

1. Glavnoye upravleniye mukomol'noy, krupyanoy i kombikormovoy promyshlennosti.
(Electric motors, Polyphase)

ORZHEKH	OVSKIY, A. Minzhener.		
	Some problems in the flour and feed indust		
	1. Rosglavmika.	(Electric motors)	

ORZHEKHOVSKIY, A.

Simple method for determining the load coefficient of asynchronous electric motors. Muk-elev.prom. 26 no.2:8-10 F 160. (MIRA 13:6)

1. Nachal'nik otdela energetiki Ministerstva khleboproduktov RSFSR.

(Electric motors, Induction)

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ORZHEKHOVSKIY, A., inzh.

Starting synchronous electric motors equipped with exciters permanently connected to the rotor winding. Muk.-elev. prom. 26 no.6:28-29 Je '60. (MIRA 13:12)

1. Nachal'nik Otdela energetiki Ministerstva khleboproduktov RSFSR. (Mectric motors, Synchronous)

OFZHEKHOVSKIY, F.I., gazovshchik

Trouble-free operation of blast furnaces and air blowers. Metallurg
8 no.3:9 Mr '63. (MIRA 16:3)

1. Metallurgicheskiy zavod imeni Petrovskogo.
(Blast furnaces)

BUTTON SECRETARIO CONTRACTOR CONT

BUGAYEV, Aleksey Alekseyevich, tokar'; IZVEKOV, Arkadiy Ivanovich, master elektrikov; TBET'YAKOV, Eduard Aleksandrovich, inzh.-tekhnolog; ORZHEKHOVSKIY, Pavel Iosifovich, slesar'; LITUS, Il'ya Sil'vestrovich; BABANOV, Nikolay Fedorovich, starshiy master; SYRODOYEV, Aleksandr Konstantinovich, mekhanik; TERENIK, Mikhail Semenovich; LADYGIN, Aleksandr Iosifovich

From the rostrum of a plant meeting. Izobr.i rats. no.12:24-28
D '58.

(MIRA 11:12)

1. Novo-Kramatorskiy mashinostroitel'nyy zavod (for all). 2. Mekhanicheskiy tsekh No. 5 (for Bugayev). 3. Mekhanicheskiy tsekh No. 7, predsedatel' tsekhovogo soveta Vsesoyuznogo obshchestva izobretateley i ratsionalizatorov (for Izvekov). 4. Upolnomochennyy Byuro ratsionalizatorov i izobretateley v l-m mekhanicheskom tsekhe (for Tret'yakov). 5.

Mekhanicheskiy tsekh No.7 (for Orzhekhovskiy). 6. Rukovoditel' sektsii sodeystviya izobretatel'stvu i ratsionalizatsii Soveta veteranov truda (for Litus). 7. Fasonnoliteynyy tsekh No.1 (for Babanov, Syroyedov).

8. Nachal'nik otdela tekhnicheskoy informatsii i izobretatel'stva (for Terenik). 9. Predsedatel' zavodskogo soveta Vsesoyuznogo obshchestva izobretateley i ratsionalizatorov (for Ladygin).

(Kramatorsk--Machinery industry)

L 21205-65 EVT(d)/EPA(s)-2/EVT(m)/EWP(w)/EPF(c)/EWA(d)/EWP(v)/T/EWP(t)/ EVP(k)/EWP(h)/EPA(bb)-2/EWP(b)/EWP(1) Pf-4/Pr-4/Pt-10 IJP(c)/ASD(m)-3/ ACCESSION NR: AP5000943 AS(mp)-2 JD/HW/DJ S/0136/64/000/012/0067/0071

AUTHOR: Gurevich, Ya. B., Orzhekhovskiy, V.L.

TITLE: Friction during hot rolling of metals

SOURCE: Tsvetnyye metally, no. 12, 1964, 67-71

TOPIC TAGS: rolling friction, hot rolling, vacuum rolling, homogenizing, refractory metal, vacuum working, surface film, surface finish, oxide film

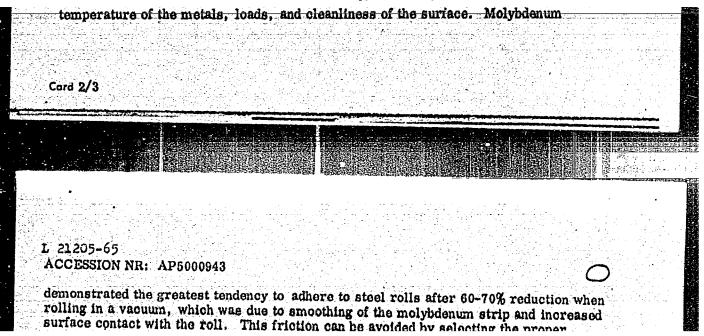
ABSTRACT: Experiments were carried out on a vacuum rolling mill to determine the effect of rolling on external friction. Rolling was done in a vacuum of 10<sup>-5</sup> mm Hg or in an argon atmosphere. Before rolling, the metals (Fe/Ni/Ti, electrical steel, Mo, ) Nb) were homogenized and the surface machined. The coefficient of friction was determined during forward rolling in the 1000-1200C temperature range with a change in atmospheric conditions (medium) of heating and rolling. It was found that on changing from hot rolling in a vacuum, where oxidation was virtually absent, to the ordinary hot deformation conditions in air, there was a 1.5-2.0 fold decrease in the coefficient of friction for Fe, Ni, Mo, Nb and a 1.5 fold increase for Ti and electrical steel. The boundary conditions at the contact surface played a vital part in external friction and therefore, when examining

Card 1/3

L 21205-65 ACCESSION NR: AP5000943

2

the quantitative and qualitative aspects of friction, the thickness of the oxide films, the temperature, and the medium were taken into account. Generally, thin surface films, scale, lubricants for the processed metal itself, lowered the coefficient of friction by reducing adhesion in the contact zone and by preventing seizing. The oxide MoO<sub>3</sub>, formed on heating molybdenum, has a melting point of 795C and acted as a natural lubricant, lowering the coefficient of friction. However, as the temperature increased from 1000 to 1200C, the effectiveness of the lubricating action decreased owing to increasing volatility of the oxide. The melting point of the oxides of all other investigated metals exceeded the maximal rolling temperature and reduced the adhesion force by shielding the metal surface against direct contact with the rolls. In this case, unlike hot rolling in a vacuum, shearing occurred in the scale (oxide) layer. Since the shear strength for Fe, Ni, and Nb in the scale layer was less than in the base metal, this scale acted as a solid lubricant, lowering the coefficient of friction. The opposite relation was found for electrical steel and Ti, probably due to the opposite effect of the oxides on the coefficient of friction. Seizing and adhesion of metals depended on the nature and



ASSOCIATION: none

SUBMITTED: 00 ENCL: 00 SUB CODE: IE MM

NO REF SOV: 009 OTHER: 001

PAVLOV, I.M.; GUREVICH, Ya.B.; ORZHEKHOVSKIY, V.L.; SHELEST, A.Ye.;

BÁSHCHENKO, A.P.

Effect of conditions of titamium heating on the indices of hot rolling. TSvet. met. 35 no.7:75-79 Jl '62.

(Titanium)

(Rolling (Metalwork))

### 5/279/63/000/001/001/023 E193/E383

AUTHORS:

Paylov, I.M., Orzhekhovskiy, V.L., Gurevich, Ya.B. Shelest, A.Ye. (Moscow)

TITLE: The effect of the roll material and surface finish on some parameters of hot-rolling in vacuum

PERIODICAL: Akademiya nauk SSSR. Izvestiya. Otdeleniye tekhnicheskikh nauk. Metallurgiya i gornoye delo, no. 1, 1963, 14 - 17

TEXT: Cast iron and steel (UX15 (ShKhl5) and 3X2B8 (5Kh2V8)) rolls, 85 mm in diameter, were used in the experiments conducted in a vacuum of 10 mm Hg on steel 20 test pieces, preheated to 1100 °C. Various surface finishes of the rolls, corresponding to class 4, 7 and 10 of the degree of flatness (as specified in FOCT (GOST) 2789-59) were obtained by turning, grinding and polishing the rolls. Test pieces with various surface finishes were prepared by grinding, milling or planing in either longitudinal or transverse directions. A constant reduction of 30% per pass was used in the experiments conducted at a rolling speed of 6.5 m/min. The roll pressure, roll torque, peripheral roll speed, forward

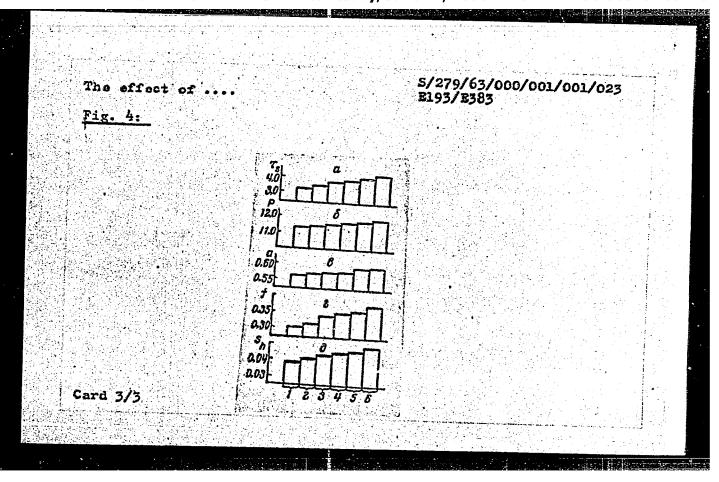
The effect of ....

S/279/63/000/001/001/023 E193/E383

slip and the speed of metal leaving the rolls were measured in each experiment. The lateral-spread coefficient was calculated on the basis of the constant-volume law. The friction coefficients were determined with the aid of a braking device and calculated from data on the forward slip. Some of the typical results obtained on ground test pieces are reproduced in Fig. 4, where the histograms show the variation in (a) friction force \( \gamma\), kg/mm, (b) roll pressure P, kg/mm, (b) lateral-spread coefficient a, (c) friction coefficient f and (d) forward slip S, blocks 1-6 relating to: 1 - ground cast-iron rolls; 2 - turned cast-iron rolls; 3 - polished steel Shkhl5 rolls; 4 - ground steel Shkhl5 rolls; 5 - ground steel Shkhl5 rolls; 6 - turned steel Shkhl5 rolls. The general conclusion was that the friction coefficient in hot rolling was affected more by the material and surface finish of the rolls than by the surface condition of the metal rolled. There are 4 figures.

SUBMITTED: July 17, 1962

Card 2/3



L. 12937-63 EWP(k)/EWP(q)/EWT(m)/BDS AFFTC/ASD Pf-1 JD/HM/HW/JG ACCESSION MR: AP3002391 S/0279/63/000/003/0123/0126 AUTHOR: Pavlov, I. M. (Moscow); Bashchenko, A. P. (Moscow); Gurevich, Ya. B. (Moscow); Orzhekhovskiy, V. L. (Moscow); Shelest, A. Ye. (Moscow)

TITLE: Dependence of the friction coefficient on temperature and ambient medium in rolling of iron, titanium, molybdenum, and niobium Accession of the friction coefficient on temperature and ambient medium in rolling of iron, titanium, molybdenum, and niobium Accession of the friction coefficient on temperature and ambient medium in rolling of iron, titanium, molybdenum, niobium, niobium, niobium, niobium, niobium, niobium, friction coefficient, temperature dependence, scale

ABSTRACT: The temperature dependence of the friction coefficient in the hot rolling of iron, titanium, molybdenum, and niobium under different conditions has been studied. Specimens were rolled at a constant speed of 6 m/min at a temperature varying from 800 to 12000 in a vacuum, in an argon atmosphere (0.005% 02, 0.01% N), or in the air. Test results showed that with rolling in the friction coefficient/for iron, which is about 0.38 at 8000, increases to a maximum of 0.45 at 9000 and then decreases gradually to 0.22 at 12000.

L 12937-63 ACCESSION NR: AP3002391

The initial increase is explained by the decreasing resistance of iron to deformation, and the subsequent decrease, by the effect of iron scale, which softens appreciably above 10000 and acts as a lubricant. The friction coefficient of titanium increases slightly as temperature increases from 800 to 900C, probably owing to some peculiarities of the α-to-β-transformation. Increasing the temperature to 12000 increases the friction coefficient, probably because of decreasing specific pressure. Titanium scale does not soften in the temperature range investigated and hence does not act as a lubricant but rather increases the friction. The increase in the friction coefficient of molyodemum rolled in air, from about 0.35 at 10000 to 0.45 at 12000, is probably caused by the increasing surface roughness associated with the increasing volatility of molybdenum oxides and the consequent surface cleanliness. The friction coefficient of niobium in air drops from 0.42 at 10000 at 0.37 at 12500, owing to the action of the scale which, in this temperature range, spreads on the metal and forms a dense, smooth surface. The effect of the scale on the relationship of the rolling temperature and friction coefficient is confirmed by the data on rolling in vacuum or in argon (the latter corresponds roughly to a vacuum of 0.1 mm Hg). As atmospheric pressure decreases from 760 to 0.00001 mm Hg, the friction coefficient of titanium decreases, while those of iron, molybdenum, and

Cord 2/3

L 12937-63
ACCESSION NR: AP3002391

niobium increase. The changing conditions of contact friction should thus be taken into account in developing the technology of the hot rolling of refractory metals in vacuum or an inert atmosphere. Orig. art. has: 3 figures and 2 formulas.

ASSOCIATION: none

SUBMITTED: 27Jul62 DATE ACQ: 12Jul63 ENGL: 00

SUB COME: MA, ML NO REF SOV: Oll OTHER: OOO

ACCESSION ER: AF3000003

AUTHOR: Pavlov, I. M.; Shelest, A. Ye; Gurevich, Ya; B.; Orzhekhovskiy, V. L.;

Bashchemko, A. E.

TITLE: Hot rolling of michium in vacuum and in a protective atmosphere

SCURCE: Tsvetny\*ys metally, no. 5, 1963, 63-67

TOPIC TAGS: nichium rolling, rolling in air, rolling in vacuum, rolling in argon, exidation, sealing, surface hardness, spread, forward alip, friction, roll

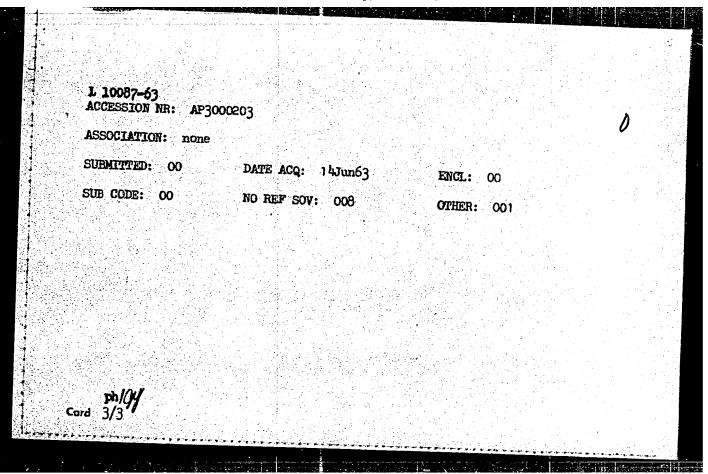
ABSTRACT: The effect of temperature and environment on the behavior of Mb in hot out of rolled plate were vacuum (approximately 10 sup =4 mm Hg) ammended at mens were heated and rolled in vacuum (approximately 10 sup -5 mm Hg) or in argon, in air, and several were heated and rolled in applies evacuated to 10 sup -2 mm Hg) and rolled.

Card 1/3

L 10087-63 ACCESSION NR: AP3000203

intensive sealing and a sharp increase of surface hardness due to the absorption of active gases, especially oxygen. No held for 90 min in air at 1100C had a surface hardness of approximately 310 kg/mm sup 2 compared with an initial hardness of approximately 130 kg/mm sup 2. Heating in vacuum or in evacuated ampules under the same conditions increased the surface hardness only to appróximately 140 or 160 kg/mm sup 2. Higher temperature and prolonged holding increased surface hardness and the depth of oxygen penetration. Spread, forward slip, specific friction, and the friction coefficient tend to decrease in rolling in air and are generally lower than in rolling in vacuum; specific roll pressure and torque decrease with increasing temperature but are higher than in vacuum. In vacuum, spread tends to increase with increasing temperature, while forward slip remains constant. Rolling in argon occupies an intermediate position between vacuum and air rolling with regard to the effect on rolling parameters. Intensive exidation of specimens heated in evacuated ampules occurred during rolling in air. It is therefore recommended to heat, roll, and cool niobium in vacuum, Orig. art. has: 7 figures.

Card 2/3



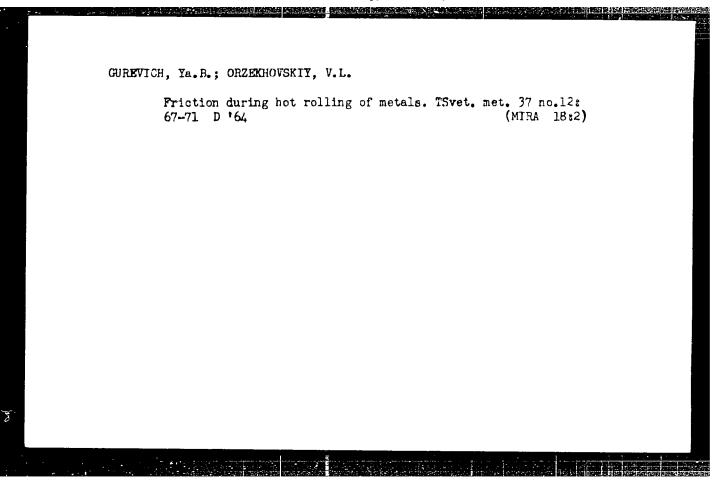
# ORZHEKHOVSKIY, V.L.; FATLAV, 1.S.; JAREVICH, Ya... Investigation initial integlerangerature deficiention of high-meltion metics. Law. Tys. under. zav.: mem. met. o.m., 988-91 U.S. (MicA 16.11) 1. Abst. variy institut static spinvov, TSentral by manchediseledovatelloky institut memory metallurgii i Institut metallurgii im. A.Albaykova.

CONTROL TO A PROPERTY OF THE P

PAVLOV, I.M.; GUREVICH, Ya.B.; SHELEST, A.Ye.; ORZHEKHOVSKIY, V.L.;
BASHCHENKO, A.P.

Investigating certain conditions for the hot rolling of molybdenum, in vacuum, in an argon atmosphere, and in air.

TSvet.met. 36 no.2:68-71 F '63. (MIRA 16:2)
(Molybdenum) (Rolling (Metalwork)) (Protective atmospheres)



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L 2971-66 ENT(m)/ENP(w)/EPF(c)/ETC/EPF(n)-2/ENG(m)/T/ENP(t)/ENP(k)/ENP(b)/ENA(c) UR/0370/65/000/004/0137/0143	
L 2971-66 EWT(m)/EWP(W)/AFF(C)/DIJ/HW/JG UR/0370/65/000/004/0137/0145	
L 2971-00 ENT(111/201 TJP(c) JD/HM/JG UR/03/0705/000705 75 ACCESSION NR: AP5021500 TJP(c) JD/HM/JG 669.018.29	• .
	- ]
Orzhekhovskiy, V. Lis Arbeton,	
AUTHOR: Gurevich, Ya. B. (Moscow); Orzhekhovskiy, V. L. (Moscow)  TITLE: Effect of the conditions of hot plastic deformation on the structure and titanium, and titanium	
TITLE: Effect of the conditions of molybdenum, niobium, and titanium properties of molybdenum, niobium, and titanium	
Notally, no. 4, 1903, 137	
SOURCE: AN SSSR. Izvestiya. Metally, no. 4, 1965, 137-143  SOURCE: AN SSSR. Izvestiya. Metally, no. 4, 1965, 137-143  TOPIC TAGS: molybdenum, 'niobium, titanium, metal plastic deformation, metal hot  TOPIC TAGS: molybdenum, 'niobium, titanium, metal plastic deformation, metal hot  TOPIC TAGS: molybdenum, 'niobium, titanium, metal plastic deformation, metal hot  TOPIC TAGS: molybdenum, 'niobium, titanium, metal plastic deformation, metal hot	
TOPIC TAGS: molybdenum, 'niobium, titanium, metal plastic deformation, metal TOPIC TAGS: molybdenum, 'niobium, titanium, metal plastic deformation, metal structure, metal mechanical property, vacuum rolling, inert gas rolling	
ABSTRACT: An investigation has been made of the gas content, structure, and metality and titanium, hot rolled with cal properties of vacuum-arc melted molybdenum, niobium, and titanium, hot rolled with cal properties of vacuum-arc melted molybdenum, niobium, and titanium, hot rolled with cal properties of vacuum-arc melted molybdenum, or a vacuum of 5.10 <sup>-5</sup> mm Hg at temperatures cal properties of 50% in air, argon, or a vacuum of 5.10 <sup>-5</sup> mm Hg at temperatures cal properties of 50% in air, argon, or a vacuum of 5.10 <sup>-5</sup> mm Hg at temperatures cal properties of 50% in air, argon, or a vacuum of 5.10 <sup>-5</sup> mm Hg at temperatures cal properties of vacuum-arc melted molybdenum, niobium, and titanium, hot rolled with	
ABSTRACT: An investigation has been made of the molybeaum, and titanium, not folice and the molybeaum, niobium, and titanium, not folice the call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice the call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties of vacuum-arc melted molybeaum, niobium, and titanium, not folice and call properties a	
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up to 800—1200C. Hot rolling in air appreciation in the oxygen up to 800—1200C. The greatest increase was in	d
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Card 1/2	

1 2971-66

ACCESSION NR:

during heating and rolling in vacuum. Heating and rolling of titanium and niobium in an argon atmosphere, as well as heating in vacuum with subsequent rolling in air, resulted in gas absorption to a degree intermediate between those produced with hot rolling in vacuum and in air. Niobium and titanium hot rolled in vacuum were satisfactorily cold rolled at room temperature. However, in niobium and titanium hot rolled in air, a more or less satisfactory plasticity in cold rolling was achieved only after the removal of the surface gas-saturated layer, which was about 1 mm thick. An additional hot rolling in vacuum or in air at 1200C (plobium and molybdenum) or at 1100C (titanium) with a total reduction of 80% resulted in some fragmentation of the a -phase of titanium. The recrystallized structure of molybdenum and niobium with almost equiaxial grains became fibrous, with the grains elongated in the direction of rolling. Niobium and titanium hot rolled in vacuum had lower tensile and yield strengths and higher ductility than after rolling in air. The metals rolled in air failed in a brittle manner; those rolled in vacuum had a ductile fracture. Rolling in vacuum or in air produced no significant difference in the mechanical properties of molybdenum. Orig. art. has: 5 figures and 3 tables. [MS]

ASSOCIATION: none

SUBMITTED: 10Nov64

NO REF SOV: 007

Cord 2/2 BVK

ENCL: 00

OTHER: 001 SUB CODE:

ATD PRESS:

APPROVED FOR RELEASE: Wednesday, June 21, 2000

CIA-RDP86-00513R001238

L 63778-55 - ENT(m)/ELF(=)-2/ENG(m)/ENA(d)/ENA(3)/ENP(R)/ENP(B)/ENA(0) 170(3) UT/0136/65/000/007/0076/0081 ACCESSION NIN: AP5017607 669.28/29:621.771.2 AUTHOR: Gurevich, Ya. B.; Bashchenko, A. P.; Orzhekhovskiv. V. J. TITLE: Features of the hot rolling of high-melting metals in a vacuum as well as in an inert gas atmosphere SOURCE: Tswetnyye metally, no. 7, 1965, 76-81 TOPIC TAGS: hot rolling, vacuum atmosphere, argon atmosphere, hot rolled titanium, hot rolled niobium, hot rolled molybdenum, hot rolled chromium, pure metal ABSTRACT: The advantages and disadvantages of the hot rolling of commercially pure (content of impurities: not more than 0.1%) Ti, Mo, No, and Cr in a vacuum of ~ 10-5 mm Hg are compared with their hot rolling in air and in an inert gas atmosphere (argon, containing 0.01% N2 and 0.005% 02). The experiments were performed in a specially designed setup, the hot rolling of the specimens being carried out at the rate of ~ 0.1 m/sec. The gas content, structure, and mechanical properties the specimens were investigated. It was found that in specimens hot-rolled in 12 - 4n +he hillets, whereas in specimens

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ACCESSION NR: AP5017607

heating in a vacuum of ~ 10<sup>-2</sup> mm Hg and rolling in air lead to its marked oxidation. In molybdenum, on the other hand, gas content remained the same level as the initial (10-20 cm³/g) in all cases (vacuum, argon, air). This is attributable to the extremely high volatility of molybdenum oxides, which led to the presence of surface effects only. Metallographic examinations of the metals revealed enlargement in grain size following hot rolling in a vacuum as compared with hot rolling in air. A comparison of the conditions and effect of hot rolling indicates that the best method is deformation in a deep vacuum (~10<sup>-5</sup> mm Hg) for such metals as Ti, Nb, and Cr. The hot rolling of these metals in a vacuum, as compared with their rolling in air or in argon, ensures: preservation of purity of the raw material or even some further enhancement in its purity; higher technological deformability; lower expenditures of power and energy and hence greater durability of work parts;

"APPROVED FOR RELEASE: Wednesday, June 21, 2000 CIA-RDP86-00513R001238 paratively shallow vacuum (~10°2 mm Hg) is permissible. Orig. art. nas: O ligures, 3 tables. Cord 2/3 1. 69178-50 APSO17607 ASSOCIATION: none SUB CODE: MM ENCL: 00 JUBMITTED: 00 OTHER: 000 RR REF BOV: 011 1012239 20 VOTUD 56, 18 APPROVED FOR RELEASE: Wednesday, June 21, 2000 CIA-RDP86-00513R0012

Card 3/3

ACC NR. AT7004422

SOURCE CODE: UR/0000/66/000/000/0130/0134

AUTHOR: Gurevich, Ya. B.; Ushakov, Ye. V.; Drobysheva, Ye. K.; Osipov,

V. G.; Orzhekhovskiy, V. L.

ORG: none

TIME: Plasticity of tungsten in vacuum rolling

SOURCE: AN SSSR. Institut metallurgii. Napryazhennoye sostoyaniye i plastichnost' pro deformirovanii metallov (Stress condition and plasticity during metal deformation). Moscow, Izd-vo Nauka, 1966, 130-

TOPIC TAGS: sintered tungsten, sintered tungsten rolling, sintered tungsten property, sintered tungsten structure, pander metal

ARSTRACT: The plastic properties of hydrogen-or vacuum-sintered tungsten and vacuum-arc melted tungsten have been investigated. Specimens 12 x 12 mm were sintered at 1200°C for 2 hr in a hydrogen atmosphere and then in vacuum. An ingot 50 mm in diameter was vacuum-arc melted with a consumable electrode from hydrogen-sintered tungsten. Hydrogen-sintered tungsten failed at a bendangle of 35 degrees, even at temperatures up to

Card 1/2

UDC: none

### ACC NR: AT7004422

1100°C, and remained brittle at room temperature. Cast tungsten has an elongation of 1% and reduction of area 3.5%. The respective elongation and reduction of area at 400°C were 2 and 6% for hydrogen-sintered tungsten and 3 and 5% for vacuum-sintered tungsten. The latter has the highest plasticity and can be vacuum rolled with a 61% reduction at 1300°C without failure, compared to 45% for hydrogen-sintered tungsten. Orig. art. has: 2 figures. [AZ]

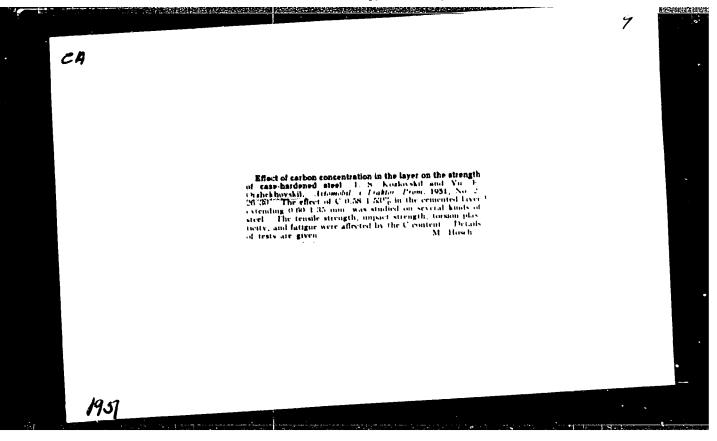
SUB CODE: 11,13/ SUBM DATE: 27Sep66/ ORIG REF: 002/ ATD PRESS:5117

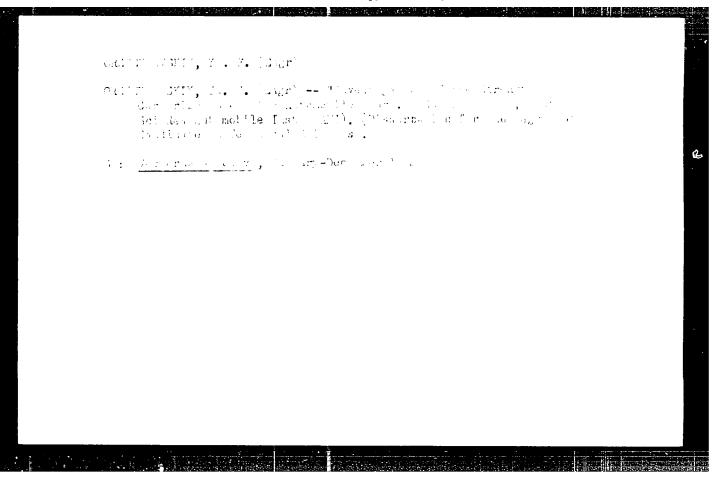
**Cord** 2/2

ORZHESHKOVSKIY, V.V., kand.med.nauk; DOVZHANSKIY, S.I., kand.med.nauk; KRUPICHEVA, A.A.

Reiter's syndrome with ankylosing spondyloarthritis. Vest. derm. i ven. 38 no.6:90-91 Je 164. (MIRA 18:6)

1. Sochinskiy nauchno-issledovatel skiy institut kurortologii i fizioterapii (dir. - zasluzhennyy vrach RSFSR N.Ye.Romanov) Ministerstva zdravockhraneniya RSFSR.





KOZLOVSKIY, I. S.; ORZHEKHOVSKIY, YU. F.

Metals - Heat Treatment

Methods for increasing the strength and decreasing the cost of neat treatment of gears. Avt. trakt. prom., No. 2, 1952.

Monthly List of Russian Accessions, Library of Congress, June 1952. UNCLASSIFIED.

- 1. KOZLOVSKIY, I. S.; ORZHEKHOVSKIY, Yu. F.
- 2. USSR (600)
- 4. Cementation (Metallurgy)
- 7. Properties of case-hardened layer in micromechanical tests, Vest. mash., 32, No. 10, 1952.

9. Monthly List of Russian Accessions, Library of Congress, February 1953, Unclassified.

## ORZHEKHOVSKIY, YU.F.

DESR/ Engineering - Cementation process

Card 1/1 : Pub, 12 - 2/16

Authors ; Kozlovskiy, I. G.; Assonov, A. D.; and Orshekhovskiy, TC. F.

Title 1 A new comented steel, Mark 30KhGT, for automobile gears

Periodical : Avt. trakt. pros. 8, 3-8, Aug 1954

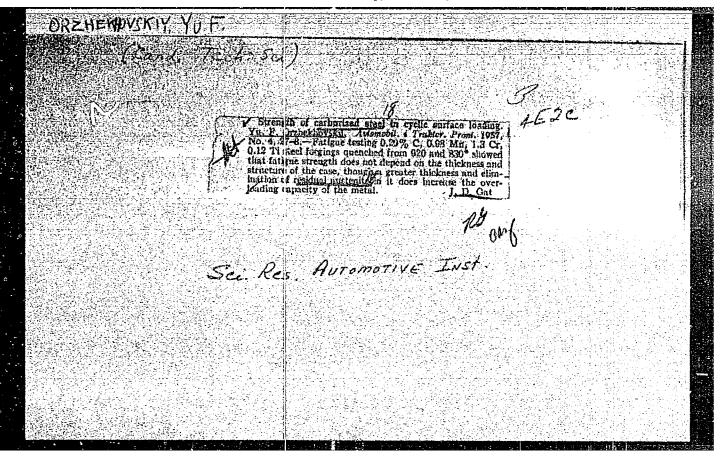
Abstract : Methods for commuting Mark 30KhGT steel were investigated. Mechanical and physical properties of the steel, and the thermal treatment of

and physical phyperties of the stear, and the thermal troubles automobile gears are described. Ten USSR references: (1945-1952).

Tables; illustrations; graphs.

Institution: .... Stalin auto Plant, Mooral

Submitted : ....



11/10

11 Just, 1454

22545 5/129/61/000/005/001/003 5/11/E152

AUTILLIAS :

rotak, Ya.h., Candidate of Technical sciences,

Orzhekhovskiy, Yu.F., Candidate of Technical Sciences

Pevzner, L.M., Candidate of Technical Sciences,

Roshchina, I.N., Engineer, and

Yermakov, V.N., Engineer.

TITLE:

Thermal-mechanical treatment of steel to give nigh

strength

PERIODICAL: Metallovedeniye i termicheskaya obrabotka metallov,

1961, No.5, pp. 2-9

TEXT: The authors point out that recently much attention has been given to combined mechanical and head treatment, by two possible methods. In one method the steel is rapidly deformed in the austenite-stable temperature range and quenched. While this improves the steel in many ways it fails to increase tensile strength. In the second method the steel is deformed at a temperature between the martensite point Md and the recrystallization temperature, and quenched. This gives increased strength with satisfactory plasticity. Results of thermal-mechanical Card 1/8

X

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S/129/61/000/005/001/003 E111/E152

Thermal-mechanical treatment of steel to give high strength

treatment are not universally successful, and there are no reliable data on the practical use of the "ausform" or "ausforming" treatment widely advertised in the USA. The object of the present work was the study of thermal-mechanical treatment of alloy structural steels to a high strength and the structure produced by the treatment. The composition of the steels was as shown in Table 1, steels A-F being melted in induction and A and E in arc furnaces: the first group were austenitized at 1000, the second at 900 °C. After cooling in a natrate bath to the deformation temperature the steels were rolled in 4-5 passes (reduction 90%), oil-quenched and tempered. To reduce cooling the work was reheated between passes and other measures taken, e.g. rolls were preheated to 100 °C. A portable magnetic instrument (developed by G. Yu. Sila-Novitskiy and T.D. Kubyshkina) was used to detect isothermal-decomposition products: if found, the specimen was rejected. After treatment specimens had a hardness Rc of 58-64 and mechanical-test pieces were prepared by spark machining and removal by grinding (temperature kept below 100 °C) Card 2/8

22545 S/129/61/000/005/001/003 E111/E152

Thermal-mechanical treatment of steel to give high strength Fig. 2 shows tensile strength of a 0.5 mm deep surface layer. kg/mm<sup>2</sup> and relative elongation as functions of carbon content for steels A, B, K and E after treatment (90% deformation at 550 °C, 4 hours tempering at 100 °C); for steel A tempering at 100 and 200 °C is shown by points 1 and 2 respectively, steels E and Z indicated by point 3. Fig. 3 shows for steel A tensile strength and elongation in relation to the 90% deformation temperature (tempering at 100 °C). The effect of variation in austenitization temperature with 90% deformation and tempering at 100  $^{\rm o}{\rm C}$  of steel A on tensile strength, Rockwell hardness and elongation is shown in Fig. 5 shows the effect of tempering temperature on these properties of the normally thermomechanically treated alloys B and (' (left- and right-hand graphs respectively). The treatment enabled a tensile strength of 280-300 kg/mm<sup>2</sup> and elongation of 6% to be obtained for the steels tested, which is better than with ordinary or stepwise hardening followed by low-temperature

tempering. As carbon content rises to about 0.5% strength of thermomechanically treated steels rises and falls with higher

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Thermal-mechanical treatment of steel to give high strength C content due to semi-brittle or brittle fracture. The best strength/plasticity combination was obtained with tempering at 100 °C. In some experiments on steel for the deformation was decreased to 50%, the results were less favourable than with the 90% deformation as regards strength, but gave high plasticity. The advantage of 50% deformation is that it can be effected at relatively high temperatures, even above the recrystallization temperature. Bend tests on 60 x 10 x 2 mm plates of steel & heated in various ways were also carried out. Electronmicroscopic study of the fine structure of thermomechanically treated steel A showed a pronounced texture and considerable refinement of martensite plates. X-ray diffraction by rotating specimens was also studied (with a 35% -50 % (URS-50I) ionization apparatus with automatic recording of intensity distribution in Feka radiation): block size of the thermomechanically treated steel was one half to one quarter that obtained with ordinary hardening. The authors conclude that structure refinement is one factor in the effectiveness of the treatment. Card 4/8

POTAK, I. M. [Potak, Ya.M.]; ORDENOVAKI, I. F. [Orzhekhovskiv, Yu. F.];
PEVZNER, L. M.; ROSCINA, I. N. [Roshchina, I. N.]; ERMAKOV, V.N.
[Yermakov, V. N.]

Thermomechanical treatment of steel for the obtainment of a high mechanical resistance. Analele metalurgie 15 no.4:114-123 0-D '61.

(Steel-Heat treatment)

Orzhekhovskiy, Yy.f.

AID Nr. 977-2 27 May

Ausforming of Structural Steels (USSR)

Yermakov, V. N., V. V. Chugunov, and Yu. F. Orzhekhovskiy. Metallovedeniye i termicheskaya obrabotka metallov, no. 4, Apr,1963, 25-29. S/129/63/000/004/006/014

Ten complex alloyed structural steels were tested for the effect of low-temperature thermomechanical treatment (ausferming) on their structure and properties. The steels had the following compositions: 1, 0.50% C, 1.2 Mn, 1.12% Si, 1.82% Cr, 2.22% Ni, 0.96% W, 0.48% Mo; 2, same as 1; with 0.55% C; 4, 0.47% C, 1.03% Mn, 1.12% Si, 1.67% Cr, 2.44% Ni, 0.95% W, 0.40% Mo, 0.009 V; 6, 0.48 % C, 1.15% Mn, 1.60% Si, 1.97% Cr, 2.15% Ni, 1.12% W, 0.45% Mo, 0.28% V (all four open-atmosphere induction-melted steels); 7, steel 1 remelted in a crucibleless vacuum furnace in a magnetic field; 9, and 10, steels 1 and 2, respectively, remelted in a consumable-electrode vacuum arc furnace; 11, electroslag remelted steel 2;

Card 1/3

AID Nr 977-2 27 May

AUSFORMING OF STRUCTURAL STEELS [Cont'd]

5/129/63/000/004/006/014

and 12 and 13, steel 4 remelted in a consumable-electrode vacuum arc furnace. The ausforming consisted of austenitizing at 1000°C, saltpeter bath or furnace cooling to 500°C, rolling in 5 to 7 passes with a total reduction of 90%, and oil quenching. This was followed by tempering at 100, 200, 300, or 400°C for 3 hrs. The specimens were encased in X18H9T stainless steel envelopes; rolls were preheated to 80-100°C. In all steels the best combination of strength and ductility—tensile strength \$\mathcal{G}\$\_0 of 280-290 kg/mm² and elongation of \$\delta = 6\$ to 9%.—was obtained by tempering at 100°C. Remelted steels generally were found to have higher strength and ductility. After tempering at 100°C the induction-melted steels had a yield strength \$\mathcal{G}\_{0.2}\$ of 200. 5 kg/mm², \$\mathcal{G}\_{0} = 266.5 kg/mm²\$, \$\delta = 5.8%\$.

In remelted steels (except for steels vacuum-remelted in a magnetic field, \$\mathcal{G}\_{0}\$ varied from 280 to 290 kg/mm², \$\mathcal{G}\_{0.2}\$ from 180 to 210 kg/mm², and \$\delta\$ from 6 to 10%. Steels conventionally hardened and tempered at 100°C in many cases showed partial brittle failure. Short-time

Card 2/3

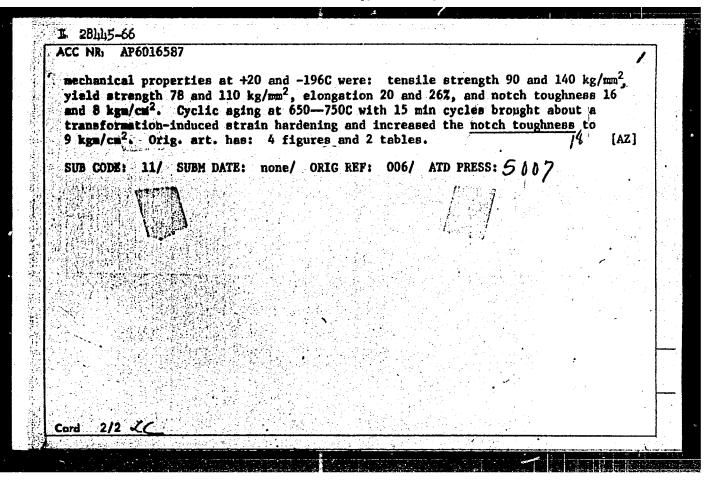
AUSFORMENT OF STRUCTURAL STEELS [Contid]

AUSFORMENT OF STRUCTURAL STEELS [Contid]

tests at elevated temperature showed that ausformed steel with 0.28% V is more heat resistant at temperatures up to 400-500°C than steel without V. Ausforming results in a considerable anisotropy of mechanical properties; transverse specimens have higher \$\mathcal{O}\_{0.2}\$ and \$\mathcal{O}\_{0.3}\$ and lower 5 than longitudinal specimens. The highest \$\mathcal{O}\_{0.2}\$ and \$\mathcal{O}\_{0.3}\$ and 306.0 kg/mm², respectively, were obtained by tempering at 200°C. The high strength of the transverse specimens is probably caused by a certain orientation of martensite needles and by the density and distribution of dislocations.

[MS]

	5-66 ENT(m)/ENP(w)/T/ENP(t)/ETI IJP(c) MJW/JD SOURCE CODE: UR/0129/66/000/005/0023/0025 AF6016587 (A, N) SOURCE CODE: UR/0129/66/000/005/0023/0025
AUTHOR	Kozlovskaya, V. I.; Potak, Ya. M.; Orzhekhovskiy, Yu. F.; Birman, S. I.
ORG:	Improving the notch toughness and ductility of martensitic stainless steel
	AND THE WAR UT I CACIDE WATER THE PROPERTY OF
	Ment lovedenive i termicheskaya obrabotka metallov, no. 3, 1900, 2322
T 1	TAGS: stainless steel, precipitation hardenable steel, martensitic steel, transformation, martensitic transformation, reversed transformation, steel
stecl	transformation, mailtenance tr
ABSTR	ACT: The possibility of using 08Kh15N5D2T (EP-410) precipitation-nardenaste activities steel (0.07%C, 15%Cr, 4.96%Ni, 1.96%Cu, and 0.18%Ti) for
-1.	- 4"/
narte	ensitic transformation was attached is formed by annealing at 9500, air coording,
	25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and Constant 25% austenite which remained stable on cooling to -1960 and -1
Cord	upc: 669.14.018.84:620.178.2



## "APPROVED FOR RELEASE: Wednesday, June 21, 2000 CIA-RDP86-00513R001238

L 0991:6-67 EMT(m)/EMP(t)/ETI IJP(c) JD •	
ACC NR: AP6035725 . SOURCE CODE: UR/0413/66/000/019/0085/0085	ı
INVENTOR: Chugunov, V. V.; Orzhekhovskiv, Yu. F.; Potak, Ya. M.	
ORG: none	
TITLE: Stainless steel. Class 40, No. 186701	
SOURCE: Izobreteniya, promyshlennyye obraztsy, tovarnyye znaki, no. 19, 1966, 85	
TOPIC TAGS: stainless steel, chromium nickel steel, molybdenum containing steel, tungsten containing steel, vanadium containing steel, niobium containing steel  ABSTRACT: This Author Certificate introduces a chromium stainless steel containing tungsten, vanadium and niobium. To improve the mechanical properties, the steel composition is set as follows (%): 0.04—0.08 carbon, 1.0 max manganese, 1.0 max silicon, 10.5—12.0 chromium, 0.6—0.8 molybdenum, 0.9—1.3 tungsten, 0.2—0.3 vanadium, 0.08—0.15 niobium, and 2.5—3.5 nickel	
SUB CODE: 11/ SUBM DATE: 30Nov64/ ATD PRESS: 5105	- -
Cord 1/1 UDC; 669.14,018,8	

## "APPROVED FOR RELEASE: Wednesday, June 21, 2000 CIA-RDP86-00513R001238

KRINETSKIY, I.I., kand.tekhn.nauk; KOTOV, Ye.N., inzh.; ORZHEL', A.D., inzh.

Investigating the nonlinear static automatic control system. Avtom.: prib. no.2:10-24 '(1. (Miñ. 14:12))

(Flectronic control)

OLEFIR, P.F., kand. tekhm. nauk; ROGANOV, F.V.; OR HEL', A.D.; MUDRAGEL',
A.V.; TIMOSHENKO, E.V.; PEROV, B.P.

Introducing an astat : control system of strip tension at coilers
on a reversing cold rolling mill. Art. 1 prib. no.4:7-11 O-D '64

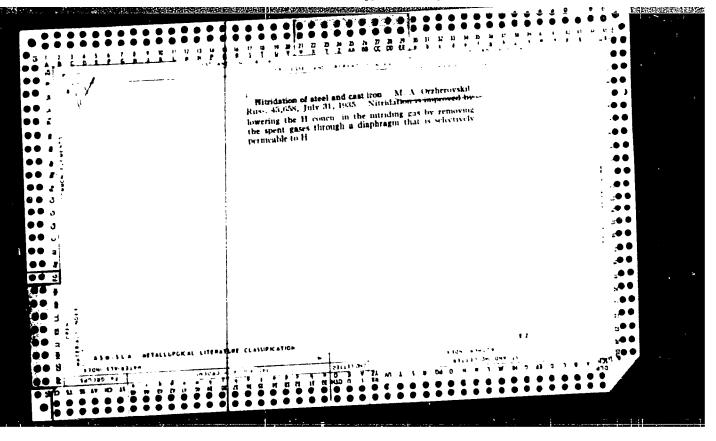
(MIRA 18:2)

# "APPROVED FOR RELEASE: Wednesday, June 21, 2000 CIA-RDP86-00513R001238

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Some intelerable depicts in the two release of records of steam bedienc. Mrs. flet (4 no. 11:20-127 D 164.	( y `	
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## "APPROVED FOR RELEASE: Wednesday, June 21, 2000 CIA-RD

CIA-RDP86-00513R001238



	USSR/Engineering Apr 48 Boilers Rust Prevention	
-	Test of the Use of a Rust Preventative on Ships of the Black Sea Shipping Company, M. Orzherovskiy, Engr, Chief, Thermal Tech Lab UChP, by pp	· .
	"Morskoy Flot" No 4	
	Describes new antirust material used in boilers of Soviet ships. Gives sketchy account of ingredients of this material, and methods for using it.	
	1/49728	

#### ORZHEROVSKIY, M. Use of a chemical foam fire extinguisher. Mor.flot 15 no.2:17-19 (MIRA 8:5) F '55. (Fire extinction--Chemical systems)

KUEITSKIT,A., inshener; ZAKHARCHUK,O., inshener; GEZHEROVSKIT,M., inshener

Cleaning by machine of oil tanks on ships. Mor. flot 15 no.6:
(MIRA 8:8)

11-12 Je 55.
(Ships--Maintenance and repair)

ORZHEROVSKII. M., ingh.; ZAKHARCHUK, O., inzh.; ZAGORUYKO, V., inzh.

Pirst marine unit for electrochemical distillation of sea water.

Mor.flot 19 no.6:29-30 Je '59. (MIRA 12:9)

1. Chernomorskoye parokhodstvo.

(Sea water, Distillation of) (Ships--Equipment and supplies)

ORZHEROVSKIY, M.; ZAKHARCHUK, O.; ZAGORUYKO, V., inzh.-konstruktor

Klectrochemical salt removal from ses water. Mor. flot 20 no.9:24(NIRA 13:10)

1. Nachal'nik basseynovoy laboratorii Chernomorskogo parokhodstva (for Orzherovskiy). 2. Starshiy inzhener-konstruktor konstruktor-konstru

SHKROB, Mikhail Samoylovich, doktor tekhn. nauk; PROKHOROV, Fedor Georgiyevich, kand. tekhn. nauk. Prinimali uchastiye: AKOL'ZIN, P.A.,
doktor tekhn. nauk; AFEL'TSIN, I.E., doktor tekhn. nauk; ZENYEVICH,
Yu.V., kand. tekhn. nauk; KVYATKOVSKIY, V.M., kand. tekhn. nauk;
KIYACHKO, V.A., doktor tekhn. nauk; GURVICH, S.M., inzh.; ORZHEROVSKIY, M.A., inzh.; STYRIKOVICH, M.A., retsenzent; MARTYNOVA, O.I.,
retsenzent; VORONIN, K.P., tekhn. red.

[Water treatment and water systems for steam-turbine electric power plants] Vodopodgotovka i vodnyi rezhim paroturbinnykh elektrostantsii. Moskva, Gos. energ. izd-vo, 1961. 470 p. (MIRA 14:9) (Feed water purification) (Steam turbines)

#### OR ZHEROVSKIY, M. Use of electric gas analyzers for the determination of petroleum product vapors in the air. Mor.flot 22 no.4:20-23 Ap 162. (MIRA 15:4)

1. Wachal'nik teplotekhnicheskoy laboratorii Chernomorskogo parokhodstva. (Air--Analysis)

(Gases--Analysis)

ORZHEROVSKIY, M., inzh.; VAYNSHTEYN, V.

Portable unit for the chemical cleaning of marine steam boilers.

(MIRA 16:5)

Mor. flot 23 no.4:27429 Ap '63.

1. Nachal'nik teplotekhnicheskoy laboratorii Chernomorskogo parokhodstva (for Orzherovskiy). 2. Starshiy inzh.-konstruktor TSentral'nogo proyektno-konstruktorskogo byuro No.3 Chernomorskogo parokhodstva (for Vaynshteyn).

(Boilers, Marine-Cleaning)

ORZHESHKOYUKIY, A. A.

PA 1/T/0

USSR/Telegraphy, Two-tone Telegraph line units Jun 1946

"Use of WT34 Tonal Telegraph Apparatus on Overhead Trunk Lines," A. A. Orzheshkovskiy, 4 pp

"Vestnik Svyazi - Elektro Svyaz'" No 6 (75)

Describes schematic and construction changes in WT34 equipment to make it more adaptable for use on overhead trunk lines. This 18-channel WT34 apparatus has the widest use on Soviet trunk lines. Well illustrated.

19770

ORZHESHKOVSKIY, A. A.

PA 19787

USSR/Telegraphy, Two-tone Telegraphy, High speed Sep 1946

"Type MTS System of Supersonic Telegraphy," A. A. Crzheshkovskiy, 3 pp

\*Vestnik Svyazi - Elektro Svyaz'\* No 9 (78)

This is a three-channel high frequency compression telephone system for use on strung wire lines. The frequency spectrum of this system comforms to the frequency spectrum of the SOS and the SOT. The apparatus was produced by the Simens - Halske Firm before the war and is at present being prepared for wide use in the Soviet Union. Well illustrated article which states some of the operational and technical aspects of this apparatus.

٧

Category: Pharmacology. Texicology. Medicinal Plants.

Abs Jour: RZhBiol., No ú, 1959, No 27859

Author : Orzheshkovskiy, V.V.

: A Study of the Action of Vegetative Chelagogues Inst Title

Orig Pub: Vrachebn. dele, 1958, No 3, 253-258

Abstract: The therapeutic action of tinctures of fruits of wild rose 7,5:100; flowers of immortelle 7,5:100;

corn silk 10:100; grass and roots of celendine

1.5: 100; flowers of marigolds 10: 100 and birch buds

100: 100 were studied on 108 patients with angiochlescytises. In all cases a cholagogue action was noted. The greatest amount of bile is secreted after introduction of celandine; the greatest decrease of

Noopital therapy cline , Kin Mis Small

V-41

ORZEHSHKOVSKIY, V.V.

Problem of the prolonged treatment of infectious nonspecific polyarthirtis with ACTH adrepal cortex hermones. Sov.med. (MIRA 11:11) 22 no.10: 108-109 0 '58

1. Iz Hauchno-issledovatel'skogo institute reventizms (dir. - prof. M.M. Shikov) Ministerstva zdravookhreneniya RSFSR. (ARTHHITIS, RHEUMATOID, ther. adrenal cortex hormones (Rus)) (ADREMAL CORTEX HORMONES, ther. use rheum, arthritis (Rus))

